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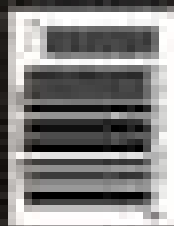
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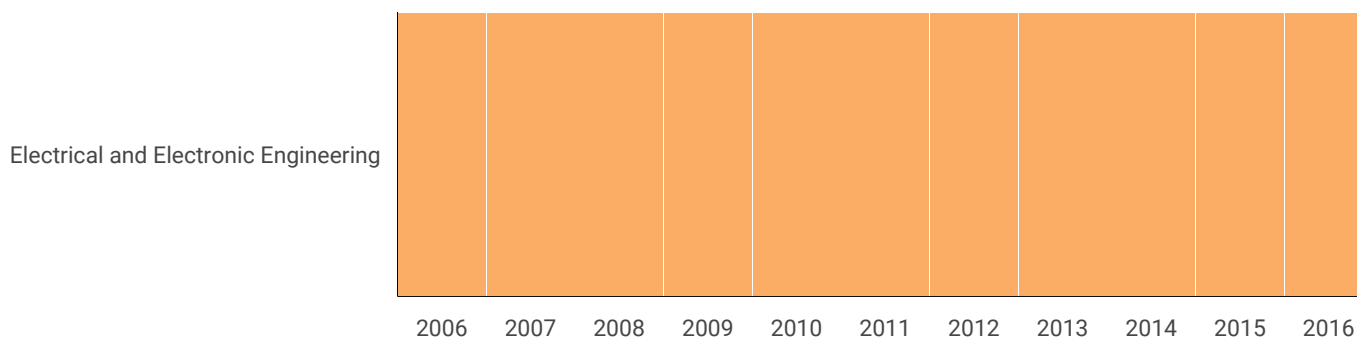
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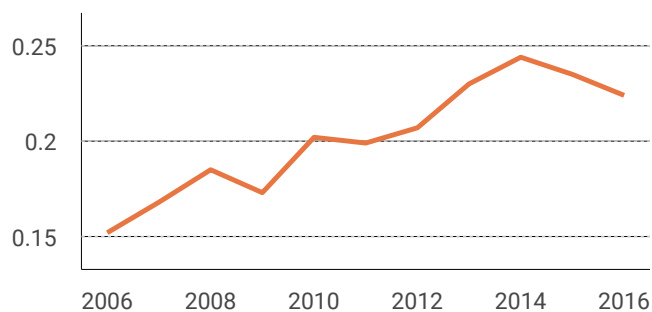
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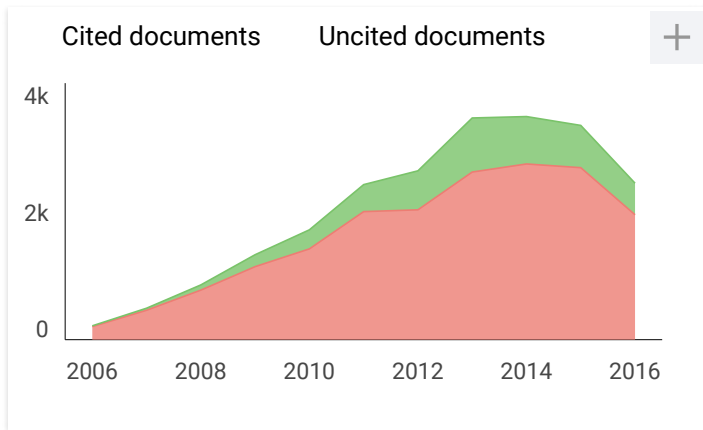
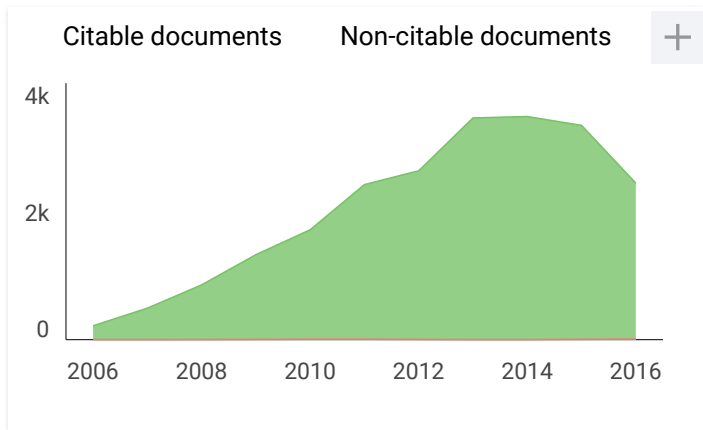
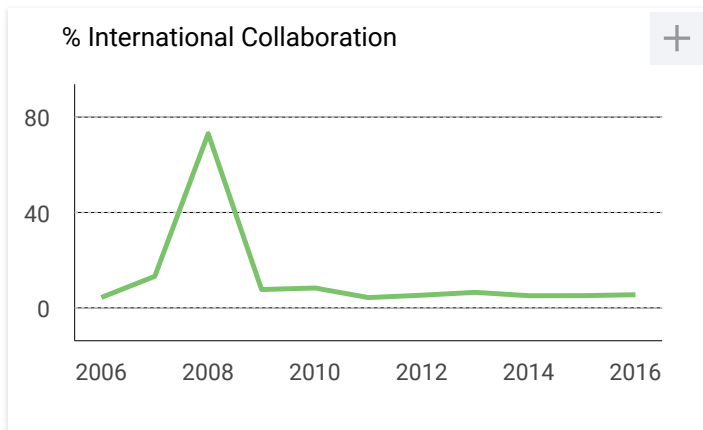
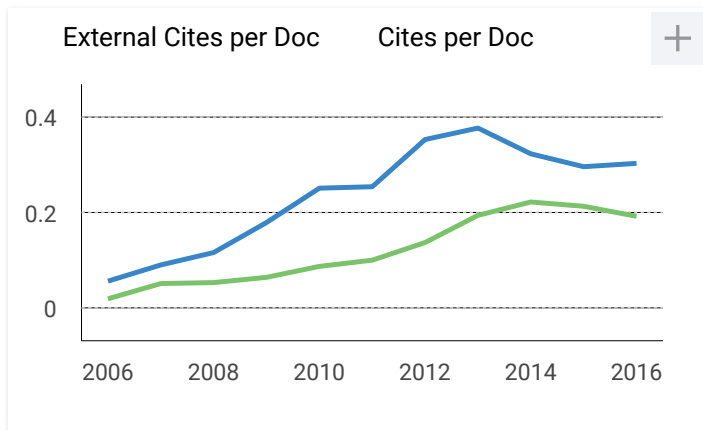
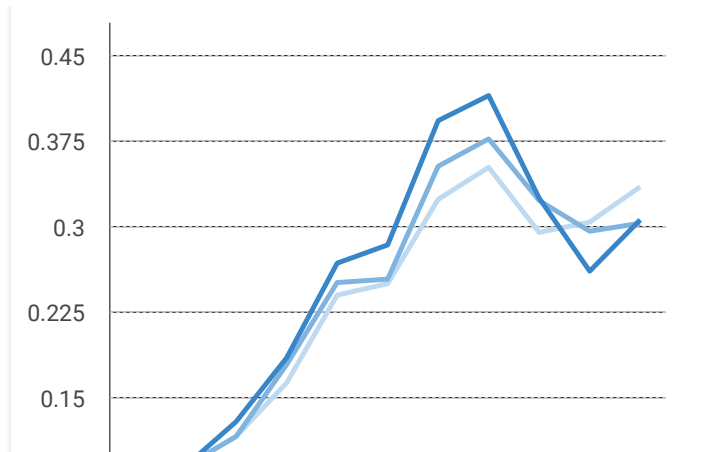
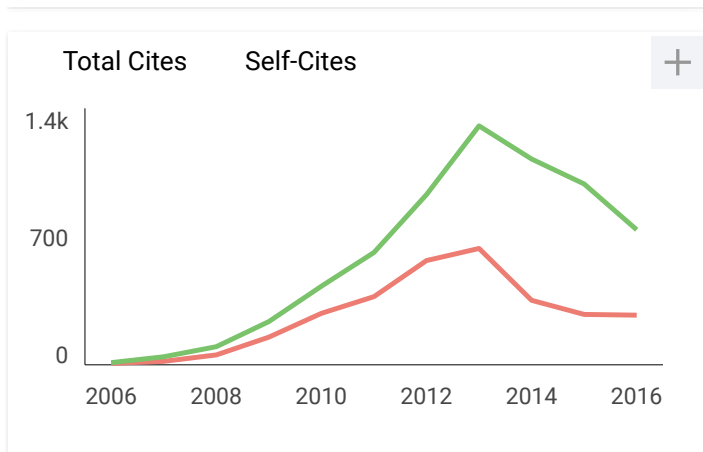
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^{1,2,3,4}Faculty of Electrical Engineering, Universiti Teknologi Malaysia, 81310 UTM, Skudai, Johor, Malaysia

An accurate fault detection and location on transmission line using wavelet based on Clarke's transformation

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e-mail: tusla@iem.pw.edu.pl
e-mail (private): tumanski@tumanski.pl

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Contents

01	Petre-Marian NICOLAE, Ileana-Diana NICOLAE, Dinuț-Lucian POPA, Marian-Ștefan NICOLAE - Active Compensation for a Driving System with Chopper and DC Motor	1
02	Leszek S. CZARNECKI, Tracy N. TOUPS - Working and reflected active powers of harmonics generating single-phase loads	7
03	Piotr BILSKI, Krzysztof LISZEWSKI, Wiesław WINIECKI - State of the art and perspectives of the artificial intelligence usability in the non-invasive identification of electrical energy appliances	11
04	Ryszard BOGACZ, Beata KRUPANEK - The basic parameters characterizing the dynamic properties of the pellistor sensor	14
05	Przemysław GRZAŚLEWICZ, Anna DOMAŃSKA - Virtual Spectrum Analyser Implementation with Intepolated DFT Algorithm in Matlab Environment	17
06	Jerzy JAKUBIEC, Beata KRUPANEK - Probabilistic model of transmission delays in homogeneous wireless system affected by disturbances	20
07	Marian KAMPIK, Krzysztof MUSIOŁ, Michał GRZENIK - Primary AC voltage standard	23
08	Ryszard KOWALIK, Łukasz NOGAL, Marcin JANUSZEWSKI, Desire RASOLOMAMPIONONA - Household electrical equipment and their features useful in methods of identification used in smart metering systems	26
09	Mariusz KRAJEWSK - Comparison of DFT and classical algorithm properties in voltage measurement using a sampling voltmeter	29
10	Beata KRUPANEK, Ryszard BOGACZ - Comparison algorithm of multimodal histograms from wireless transmission	32
11	Robert ŁUKASZEWSKI, Wiesław WINIECKI - Systems for monitoring electricity consumption in the house	35
12	Adam MARKOWSKI – Standards in the development of Building Energy Management Systems	39
13	Emil MICHTA, Robert SZULIM, Adam MARKOWSKI, Wiesław MICZULSKI - Intelligent Power Substations	42
14	Ryszard RYBSKI, Janusz KACZMAREK, Mirosław KOZIOŁ, Marian KAMPIK, Edyta DUDEK, Adam ZIÓLEK - Evaluation of the measurement system for determination of frequency characteristics of functional blocks used in AC impedance bridges	45
15	Robert SZULIM - Usage of Open - Source IEC 61850 software solutions for integration of measuring and control systems	48
16	Magdalena ŻUKOWSKA, Marcin JANUSZEWSKI, Ryszard KOWALIK - Distributed system of fault recording using data exchange via Ethernet network	51
17	Maciej A. DZIENIAKOWSKI, Paweł FABIJĄŃSKI - LCL Resonant Circuit Industrial Applications	54
18	Piotr FALKOWSKI, Marian Roch DUBOWSKI - Comparison of properties vector current regulator in the dynamic states in the AC/DC converter	58
19	Andrzej GALECKI, Arkadiusz KASZEWSKI, Lech M. Grzesiak, Bartłomiej UFNALSKI - State-space current controller for the four-leg two-level grid-connected converter	63
20	Arkadiusz GARDECKI - Computational cost-effectiveness of parallelization granularity numerical integration PECE algorithm	67
21	Agata GODLEWSKA, Andrzej SIKORSKI - A new control method of three-phase current source rectifier	70
22	Piotr GRZEJSZCZAK, Mieczysław NOWAK, Roman BARLIK - Analytical description of nonlinear capacitance of high-voltage power switches in estimating switching losses	74
23	Michał GWÓŹDŹ - Aspects of the work of a LC output filter in a power electronics voltage source	78
24	Jerzy MARZECKI, Bartosz PAWLICKI - Method of testing 110kV/MV substations development under uncertain conditions	83
25	Norbert MIELCZAREK - Effect of method with perturbation of control parameter on control of buck converter	87
26	Michał ROLAK, Mariusz MALINOWSKI - Six-phase symmetrical induction machine under fault states- modelling, simulation and experimental results	91
27	Dariusz STANDO, Przemysław CHUDZIK, Artur MORADEWICZ, Rafał MIŚKIEWICZ - Predictive control of inverter fed induction machine	96
28	Mirosław WCIŚLIK, Karol SUCHENIA - Analysis of switched reluctance motor with windings distributed	100
29	Mariusz ZDANOWSKI, Jacek RĄBKOWSKI, Roman BARLIK - Three-phase, two-level voltage source inverter with SiC Z-FETs	104
30	Anna GÓRECKA-DRZAZGA - Miniature X-Ray sources	108

PRZEGLĄD ELEKTROTECHNICZNY Vol 2014, No 11

Contents

31	Bartłomiej GUZOWSKI, Grzegorz TOSIK, Zbigniew MAKIEWICZ - Pressure Sensor Based On Optical Fiber With Reduced Coating Diameter	113
32	Michał KRYSZTOF, Tomasz GRZEBYK, Anna GÓRECKA-DRZAZGA, Jan DZIUBAN - Miniature electron microscope – concept and technology capabilities	116
33	Szymon MILCARZ, Jacek GOLEBIOWSKI - Transmission fibre-optic transducer used for a silicon structure's displacement measurement	120
34	Marek PACHWICEWICZ, Jerzy WEREMCZUK - Microprocessor device for TEWL coefficient measurement	123
35	Katarzyna SAREŁO, Anna GÓRECKA-DRZAZGA, Jan DZIUBAN - Optical detection method suitable for diaphragm silicon MEMS pressure sensors	127
36	Daniel SAWICKI, Andrzej KOTYRA - Monitoring combustion process using image classification	130
37	Piotr WARDA - Voltage-to-frequency converter simulation in LabVIEW	133
38	Tomasz WIDERSKI, Ewa RAJ, Zbigniew LISIK, Przemysław KUBIAK - Temperature Measurements of Automotive Power Electronic Equipment with Microchannels Liquid-cooling System	137
39	Michał ZABOROWSKI, Dariusz SZMIGIEL, Piotr GRABIEC - Development of REFET for Differential Measurements of pH in a Fluidic System	142
40	Piotr BATOG, Andrzej SZCZUREK - Sensor module for measurements of volatile organic compounds concentration for miniature flying platforms	147
41	Dalibor VALEK, Radomir SCUREK - Method of Selecting the Most Important Power Lines in a Transmission and Distribution Network	152
42	Makmur SAINI, Abdullah Asuhaimi Bin MOHD ZIN, Mohd Wazir Bin MUSTAFA, Ahmad Rizal SULTAN - An accurate fault detection and location on transmission line using wavelet based on Clarke's transformation	156
43	Renuga VERAYIAH, Azah MOHAMED, Hussain SHAREEF, Izham ZAINAL ABIDIN - Under Voltage Load Shedding Scheme Using Meta-heuristic Optimization Methods	162
44	Mahammad A. HANNAN, Safat B. WALI, Tan J. PIN, Aini HUSSAIN, Salina A. SAMAD - Traffic Sign Classification based on Neural Network for Advance Driver Assistance System	169
45	Galina A. SIVYAKOVA, Sergey Y. ORLOV, Waldemar WÓJCIK, Paweł KOMADA - Development of simulation model of electric drive of decoiler	173
46	Tamara SAVCHUK, Sergiy PETRISHYN, Laura SUGUROVAS, Andrzej SMOLARZ - Identification of technogenic emergency situations in railway transport using cluster analysis	177
47	Adam GŁOWACZ, Witold GŁOWACZ, Zygfryd GŁOWACZ - Diagnostics of Direct Current generator based on analysis of acoustic signals with the use of bi-orthogonal wavelet transform and nearest mean classifier	185
48	Karol WRÓBEL, Piotr J. SERKIES - Application of the model predictive control MPC to induction drive with elastic coupling	189
49	Dawid MAKIEŁA - Determining of commutation time in PM BLDC motors	193
50	Sergiej GERMAN-GALKIN, Jarosław HRYNKIEWICZ - Modular reluctance electric machine	196
51	Piotr SWIETONIOWSKI, Tomasz BINKOWSKI - The influence of temperature on optical and electrical parameters of medium and high power LEDs	200
52	Bogdan SAPIŃSKI, Stanisław KRUPA, Andrzej MATRAS - Eddy current losses and cogging force and in an MR vibration-isolator in squeeze mode	204
53	Zbigniew HANDZEL, Mirosław GAJER - Implementation of group-based genetic algorithms for economic dispatch problem in an electrical energetic system	208
54	Janusz DUDCZYK, Adam KAWALEC - The use of fractal features extracted from radar signals in the process of specific identification	212
55	Maciej SIWCZYŃSKI, Konrad HAWRON - The relationship between a reactive power and voltage source sensitivity in the frequency domain	216
56	Sławomir Andrzej TORBUS - The impact of electron mass to the measurement error of current using polarimetric sensor	220
57	Jan C. STĘPIEŃ, Zdzisław MADEJ - Analysis of Failures Duration of Rural Low-Voltage Overhead Lines	224
58	Dawid GRADOLEWSKI, Piotr TOJZA, Grzegorz REDLARSKI - Adaptive Neural Network Filter for denoising the phonocardiography signal	227
59	Krzysztof KONOPKO - The use of massively parallel processors in additive synthesis	231
60	Piotr DERUGO, Krzysztof SZABAT - A novel implementation algorithm for a fuzzy controller based on the matrix form of the controller	235
61	Konrad GRYSZPANOWICZ, Sylwester ROBAK - Analysis of the impact of photovoltaic generation source on power system voltage stability	239
62	Bartosz MINOROWICZ, Amadeusz NOWAK, Frederik STEFANSKI - Hysteresis Modelling in Electromechanical Transducer with Magnetic Shape Memory Alloy	244
63	Jakub GAŁKA, Mariusz MAŚSIOR, Michał SALASA - The concept of embedded solution for voice biometric access system	248
64	Krzysztof Andrzej WAŚOWSKI, Justyna FRYC, Adam WIĘCKO, Irena FRYC - Bicycle lighting regulations determined by the quality of vision as well as the European Union legal requirements	256

An accurate fault detection and location on transmission line using wavelet based on Clarke's transformation

Abstract. This paper presents accurate fault detection and location using wavelet based on Clarke's transformation. This study was done using Clarke's transformation method to convert current phase (three phase) signal into a two-phase current alpha and beta (current mode). The proposed method introduced the mode current to transform the signal using discrete wavelet transform (DWT) and was utilized to obtain the wavelet transform coefficients. Analysis was also conducted for other mother wavelets. The most accurate parent was wavelet Db8, with the fastest time of detection and the smallest error, whereas the largest error was found in Coif4 parent wavelet. The result for proposed method was compared with Db4, Sym4, Coif4 and Db8 and found to be very accurate

Streszczenie. W artykule opisano dokładną metodę wykrywania awarii w sieciach przesyłowych bazująca na falkowej transformacji Clarka. Sygnał trójfazowy jest przekształcany do postaci dwufazowej. Za najbardziej się do tego celu nadająca uznano falkę Db8 z najszybszym czasem wykrywania i najlepszą dokładnością. Wyniki porównano z innymi typami falek. Dokładna metoda lokalizacji awarii w sieciach przesyłowych bazująca na wykorzystaniu transformaty falkowej Clarka

Keywords: Wavelet Transformation; Fault location; Fault detection; Clarke's Transformation.

Słowa kluczowe: wykrywanie i lokalizacja awarii, transformata falkowa, transformata Clarka.

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Introduction

Fault detection and determination of the location of short circuit transmission lines have become a growing concern. There are two commonly used methods to determine the location of the fault in accordance with standard IEEE Std C37.114. 2004 [1]. The first method is based on a frequency component, and the second is based on signal interference at high frequencies where the wave theory is ignored and a shorter sampling window is used [2]. The determination of wave theory for intrusion detection was introduced by Dommel and Michess [3], where transient voltage waveform and current waveform were used to describe the graph pattern and detect fault location respectively.

C.Y.Evrenosoglu and A.Abur [4] developed a circuit defining the technical relationship between the arrival of peak measurement of, the forward and backward traveling waves which were used to predict the travel time of a transient signal transmitter (source signal) to the point affected by the fault. Wave theory is categorized under graphic patterns [5]-[7]. These are described based on the voltage and current waveform, in the form of a brief relationship between the arrival of the peak value at the measurement point of forward and backward waves.

A new approach to detect and determine fault location is introduced in this paper. It is based on Clarke's transformation which basically transforms a three-phase system into a two-phase system [8,9]. The results of this transformation are then transformed into wavelet transformation.

Wavelet transformation is a technique used to solve signal problem, based on the development of Fourier's transformation. [10]. The basic functions used in wavelet transform have band pass characteristics that make mapping similar to the mapping in the form function of time and frequency [11]. The wavelet transformation analyzes not only the frequency as in Fourier's traditional method, but also include sudden disturbances such as a transient disturbance. The wavelets generate waves and disrupt the signal frequency [12].

There are many advantages of applying a wavelet in an electric power system as mentioned in many references [13,14]. These papers present an overview comparison of Fourier; short-time Fourier and wavelet transformation,

which are examples of the application of wavelet transformation to analyze the transient power system.

In this paper, PSCAD/EMTDC [15] is used to obtain the transient signal interference from transmission lines using MATLAB, which is used to perform Clarke's transformation.

Overview of Clarke's and wavelet transformation.

A. Clarke's Transformation.

Clarke's transformation, also referred to as ($\alpha\beta$) transformation, is a mathematical transformation to simplify the analysis of a series of three phases (a, b, c). It is a two-phase circuit ($\alpha\beta 0$) stationary and conceptually very similar to the ($dq0$) transformation. The wave signal analyzer is a very useful application for the transformation.

Clarke's transformation is one of the transformation matrices, which correspond to three-phase transmission lines. A three-phase current that has a digital representation is assumed to have the form [16]

$$(1) \quad \begin{aligned} i_a(n) &= I_a \cos(n\omega T + \phi a) \\ i_b(n) &= I_b \cos(n\omega T + \phi b) \\ i_c(n) &= I_c \cos(n\omega T + \phi c) \end{aligned}$$

where T is the sampling period.

Equation (1) can be re-formed into the following matrix form (2)

$$(2) \quad \begin{bmatrix} i_\alpha(n) \\ i_\beta(n) \\ i_0(n) \end{bmatrix} = \frac{2}{3} \begin{bmatrix} \frac{1}{2} & \cos(\frac{2\pi}{3}) & \cos(-\frac{2\pi}{3}) \\ 0 & \sin(\frac{2\pi}{3}) & \sin(-\frac{2\pi}{3}) \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix} (x) \begin{bmatrix} i_a(n) \\ i_b(n) \\ i_c(n) \end{bmatrix}$$

$$(3) \quad \begin{bmatrix} i_\alpha(n) \\ i_\beta(n) \\ i_0(n) \end{bmatrix} = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix} (x) \begin{bmatrix} i_a(n) \\ i_b(n) \\ i_c(n) \end{bmatrix}$$

Therefore, the above components can be formed into matrix form [17, 18]

$$(4) \quad i_{\alpha\beta 0} = C i_{abc} = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \end{bmatrix} (x) \begin{bmatrix} i_a(n) \\ i_b(n) \\ i_c(n) \end{bmatrix}$$

where C is the famous transformation introduced by Edith Clarke [19].

Wavelet Transformation

Wavelet transformation is a refinement of the Fourier transformation, where the wavelet transform allows placement time as a frequency component within the given different signal. Sort Time Fourier Transforms is another improvement of the Fourier transform [20, 21], which uses a fixed amount of the modulation window. This is because a narrow window gives bad time resolution. Therefore, the Fourier transform is only suitable for the information signal frequency as it does not change according to time.

Continuous Wavelet Transformation.

Continuous Wavelet Transformation (CWT) is used to calculate the convolution of a signal from a modulation signal, with a window at any time to any desired scale. By giving a wave function $f(t)$, the CWT can be calculated as follows [22, 23].

(5)

$$CWT(f,a,b) = \frac{1}{\sqrt{a}} \int_{-s}^s f(t) \varphi^* \left(\frac{t-b}{a} \right) dt$$

where a and b are the constants and constant scale transnational, CWT (f, a, b) is the continuous wavelet transform of a coefficient, and φ is wavelet functions which value are not real but just for simplification purposes only. The selection of the parent wavelet will be adapted to the needs of the wavelet coefficients.

Discrete Wavelet Transformation

Discrete Wavelet Transformation (DWT) is considered relatively easy to implement compared to CWT. The coefficient of the discrete wavelet transformation of a wave can be obtained by applying the DWT as given by equation (6) [24, 25].

$$DWT(f,m,k) = \frac{1}{\sqrt{a_0^m}} \sum_k f(k) \varphi^* \left[\frac{n - ka_0^m}{a_0^m} \right] \quad (6)$$

where the parameters a and b in equation (6) are replaced as a_0^m , ka_0^m and where k and m are positive integer variables. From just a few samples of WTC taken, the implementation of DWT decomposition is essentially based on a Mallat algorithm [26,27].

(i)

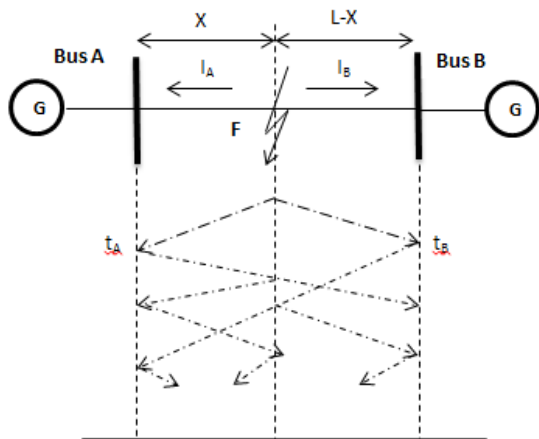


Fig.1. Bewley Lattice diagram of the transmission line

The proposed Algorithm

The simulations were performed using PSCAD, and the simulation results were obtained from the fault current signal.

The steps performed in this study were:

(ii) Finding the input to the Clarke transformation, wavelet transformation, and the signal flow of PSCAD converted into m.files (*. M) and then converting this into mat. Files (*.mat) with a sampling rate of (10^5) and a frequency dependence of 0.5 Hz – 1 MHz.

(iii) Determining the data stream interference, where the signal was transformed by using the Clarke transformation to convert the transient signals into basic current signal (Mode).

(iv) Transforming mode current signals again by using DWT and WTC, which was the generated coefficient and then squared to be $(WTC)^2$ in order to obtain the maximum signal amplitude to determine the timing of the interruption.

Processing the ground mode and aerial mode $(WTC)^2$ using the Bewley Lattice diagram [28] of the initial wave to determine the fault location as shown in Fig. 1.

If

$$(7) \quad t_A = \frac{x}{v}$$

and

$$(8) \quad t_B = \frac{L-x}{V}$$

Then

$$(9) \quad x = \frac{L - \Delta t(x)v}{2} \text{ km}$$

where t_A - Time fault from bus A, t_B - Time fault from bus B; x - Calculated distance of fault location; L - Distance transmission line; V - Propagation velocity ; d - Estimation of the distance of fault location.

To determine the distance from the fault location from Bus A $\Delta t = t_B - t_A$

To determine the distance from the fault location from Bus B $\Delta t = t_A - t_B$

Error

$$(10) \quad = \left| (x-d)/L \right| (x) 100\%$$

The flowchart of the algorithm used in this study is shown in Fig. 2

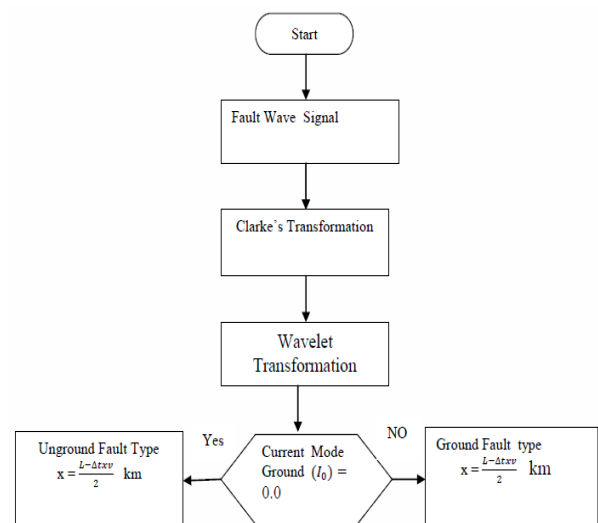


Fig. 2. Flowchart of fault detection and fault location

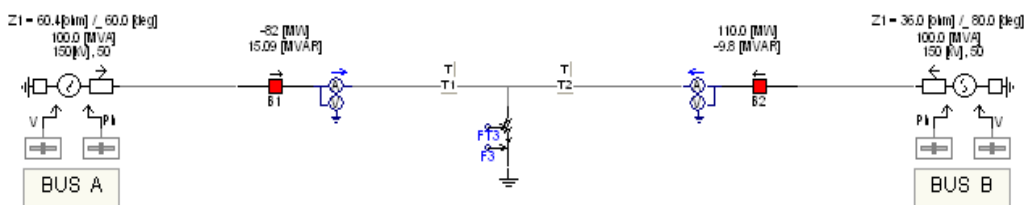


Fig. 3. Single line of the system under study using PSCAD/EMTDC

Simulation model.

The system under study is shown in Fig. 3. It consists of 150 kV transmission line 100 km in length. Two sources are connected at both sides of the transmission line edges. The system was performed using PSCAD/EMTDC software.

Transmission data:

Sequence Impedance ohm/km

Positive and negative = $0.03574 + j 0.5776$

Zero = $0.36315 + j 1.32.647$

Source Bus A $Z1 = Z2 = Z0 = 30.20 + j 52.32$ Ohm

Source Bus B $Z1 = Z2 = Z0 = 6.25 + j 35.45$ Ohm

Fault Starting = 0.22 seconds

Duration in fault = 0.15 Seconds

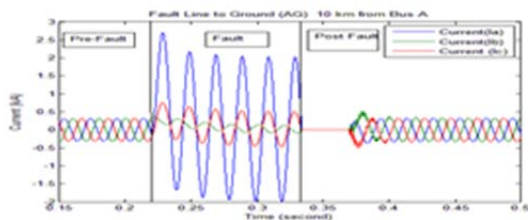
Fault resistance (R_f) = 2 ohm

Type Conductor = Chukar, diameter = 1.602 inch [29]

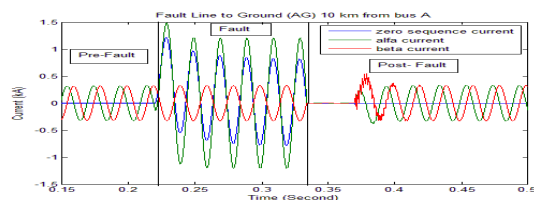
The position of the tower and the distance between the conductors were taken into account to achieve system accuracy. The conductor types used for this simulation were obtained using propagation velocity $= \frac{1}{\sqrt{LC}} = 299939.4321$ km/seconds.

Case 1: Single line to ground fault (AG), 10 km from bus A and 90 km from bus B

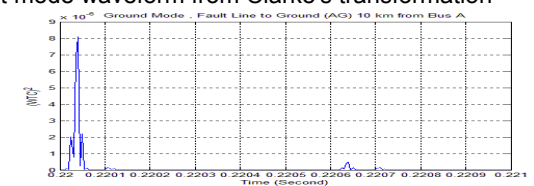
In the transient signals in Fig. 4(a). the interference was measured from Bus A. The fault current was obtained from a bus as far as 10 km, with disorder type. $I_a = 2.699$ kA, $I_b = 0.53388$ kA and $I_c = 0.7556$ kA. Fig. 4(b). shows a mode signal graph with the application of a current signal that was obtained using Clarke's transformation, with $I_\alpha = 1.484$ kA, $I_\beta = 0.5518$ kA and $I_0 = 1.216$ kA from bus A to the point of interruption of 10 km. Fig. 4(b). shows that, there was a signal waveform I_0 , which was assumed to occur due to ground fault. Fig. 4(c). shows the graph $(WTC)^2$ in the ground mode. The results of the wavelet transformation value did not indicate zero, meaning that the ground fault occurred in the first peak which is 0.22004 seconds. Fig. 4 (d). shows $(WTC)^2$ in which the peak occurred in aerial mode $(WTC)^2$ at t_A equal to 0.22004 seconds.



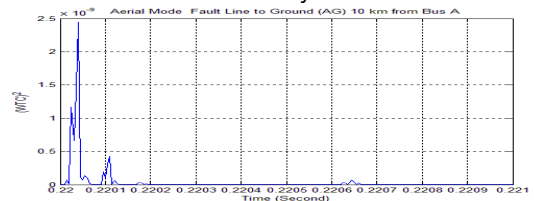
(a) Current waveform signal original



(b). Current mode waveform from Clarke's transformation



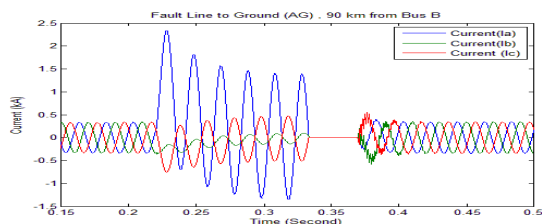
(c). Ground mode for wavelet mother Sym4



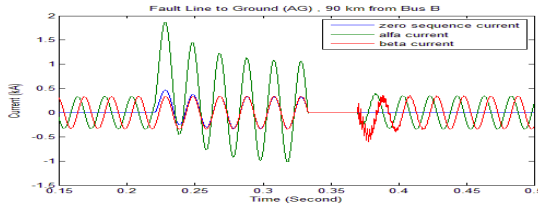
(d). Aerial mode for wavelet mother Sym4

Fig. 4. Single line to ground fault (AG) 10 km from bus A for case 1

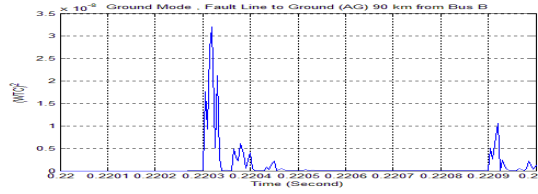
Fig. 5(a). presents the transient interference signals, measured from Bus B, obtained from the bus fault current interruption that was located 90 km from bus B, with $I_a = 2.340$ kA, $I_b = 0.352$ kA and $I_c = 0.5579$ kA. Fig.. (5b). shows a graph of the signal mode Clarke transformation, with signal $I_\alpha = 0.930$ kA, $I_\beta = 0.358$ from bus B to the point of interruption which occurred at 90 km at $I_0 = 0.4712$ kA is obtained. It was assumed that there was interference on the ground fault type. Fig.. 5(c) shows the graph $(WTC)^2$ in the ground mode, where in the results of the wavelet transformation mode at ground zero, the value did not indicate zero, meaning the ground fault occurred in the first peak at 0.22032 seconds. In Fig.. 5(d). the graphs show the $(WTC)^2$ in Aerial mode, in which the peak occurred in $(WTC)^2$ which is $t_B = 0.22031$ seconds



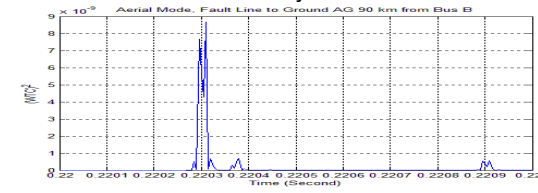
(a). Original signal of current waveform



(b). Current mode waveform from Clarke's transformation



(c). Ground mode for wavelet mother Sym4

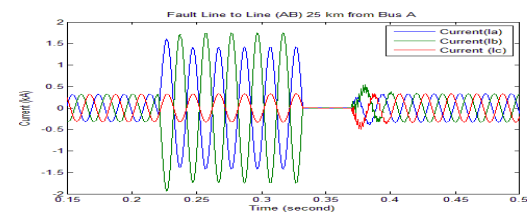


(d). Aerial mode for wavelet mother Sym4

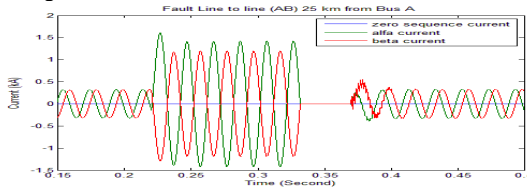
Fig. 5. Single line to ground fault (AG) 90 km from bus B for case 1

Case 2 : Line to line fault (AB), 25 km from bus A and 75 km from Bus B

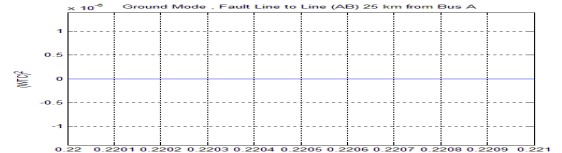
In Fig. 6(a). the graph shows the transient interference signals measured from bus A, where the fault current was obtained from bus A to a point where the fault was located 25 km from bus A with $I_a = 1.608$ kA, $I_b = 1.73533$ kA and $I_c = 0.3542$ kA. Fig. 6(b) shows a graph of the obtained mode signal current with $I_\alpha = 1.607$ kA, $I_\beta = 1.193$ kA and $I_0 = 0$ kA to the disturbance point of the bus located 25 km away. Fig. 6(b) shows that the current I_0 produced no signal. Therefore, it can be concluded that the above disorder was a type of ungrounded fault. Fig. 6(c) shows the graph $(WTC)^2$ on ground mode. The results of the wavelet transformation mode showed the ground zero value, meaning that this type of fault was ungrounded. Fig. 6(d) shows $(WTC)^2$ in Aerial mode where the peak occurred in $(WTC)^2$ at $t_A = 0.22009$ seconds.



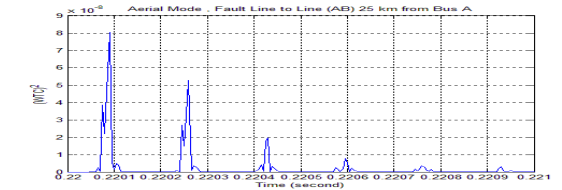
(a). Original signal of current waveform



(b). Current mode waveform from Clarke's transformation



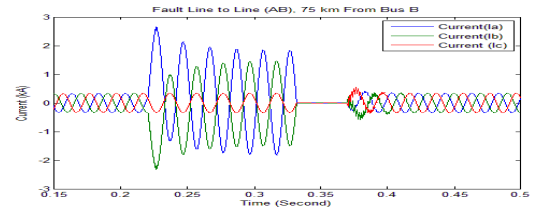
(c). Ground mode for wavelet mother Db8



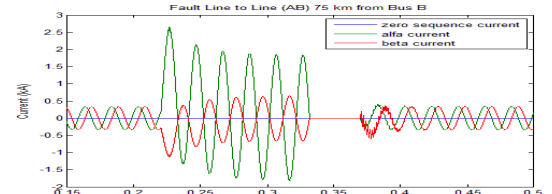
(d). Aerial mode for wavelet mother Db8

Fig. 6. Line to line fault (AB) 25 km from bus A for case 2

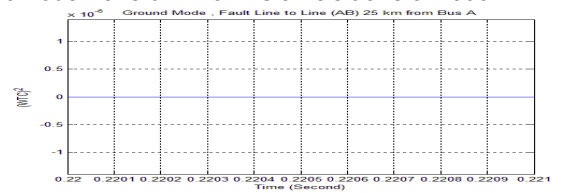
Fig. 7(a) signifies the transient signal interference graph measured from bus B, obtained from the bus fault current interruption to point B for 75 km with $I_a = 2.654$ kA, $I_b = 1.4733$ kA and $I_c = 0.5468$ kA. Fig.7(b) shows a graph of the signal mode with a current of $I_\alpha = 0.2654$ kA, $I_\beta = 0.6473$ kA and $I_0 = 0$ on bus B to the point of disorder at 75 km. Fig. 7(b). shows that the current $I_0 = 0$, thus suggesting that the disorder was a disturbance at the ungrounded fault. Fig. 7(c). shows the graph $(WTC)^2$ in ground mode. The results of wavelet transformation mode showed ground zero value, which means that this was an ungrounded fault. Fig. 7(d)..shows $(WTC)^2$ in aerial mode in which the peak occurred at $(WTC)^2$ at $t_B = 0.22026$ seconds.



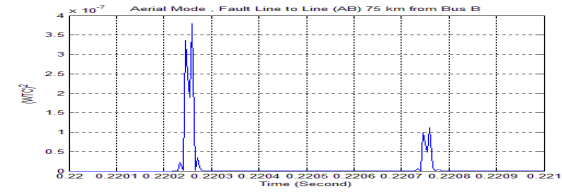
(a). original signal of Current waveform



(b). Current mode waveform from Clarke's transformation



(c). Ground mode for wavelet mother Db8



(d). Aerial mode for wavelet mother Db8

Fig. 7. Line to line fault AB located at 75 km from bus B for case 2

Discussion and Result

Fig. 8 shows that the fault detection column Db4 had a long-time duration of 0.00018 seconds for time fault detection, while Sym4 and Coif4 have similar time for fault detection of about 0.000165 seconds. Db8 had a better time for fault detection compared to others at about 0.00016 seconds. The percentage of error in fault location for different type of mother wavelet is shown in Table 1. shows more detailed results, including the error calculation of the single line to ground fault. This shows that Db4, Sym4 and Db8 had the same percentage error for the distance of 10 km and 90 km of the transmission line, whereas at 25 km, Db8 had a better performance than the rest. In contrast, for 75 km transmission line, Db4 and Sym4 had less percentage error than Db8

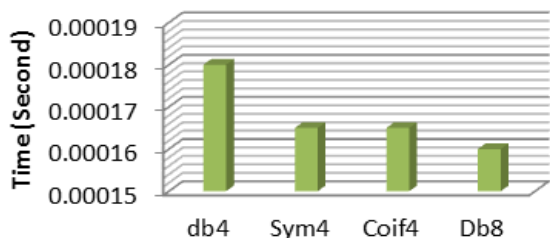


Fig.8. Fault time detection (second

Table 1. Percentage error in Fault Location for different type of Mother Wavelet, $R_f = 2 \text{ Ohm}$ and fault inception angle = 0 (degree)

Type Of Fault	Actual Point of Fault (km)	Db4		Coif4		Syms4		Db8	
		Calculated point of Fault (km)	Error = $(x-d)/L * 100\%$	Calculated point of Fault (km)	Error = $(x-d)/L * 100\%$	Calculated point of Fault (km)	Error = $(x-d)/L * 100\%$	Calculated point of Fault (km)	Error = $(x-d)/L * 100\%$
LG (AG)	10	9.51	0.419	12.52	2.051	9.51	0.419	9.51	0.419
	25	24.51	0.495	26.01	1.001	24.51	0.495	24.51	0.495
	75	74.45	0.258	73.99	1.005	74.45	0.258	75.49	0.495
	90	90.49	0.492	88.99	1.080	90.49	0.492	90.49	0.492
LL (AB)	10	9.51	0.419	11.01	1.001	9.51	0.419	9.51	0.419
	25	24.51	0.495	26.01	1.001	24.51	0.495	24.51	0.495
	75	75.49	0.495	73.99	1.001	75.49	0.495	75.49	0.495
	90	90.45	0.492	86.69	1.307	90.49	0.492	90.49	0.492
LLG (BCG)	10	9.51	0.419	10.86	0.857	9.51	0.419	9.51	0.419
	25	26.01	1.001	26.01	1.005	24.51	0.495	24.51	0.495
	75	73.99	1.001	73.85	1.155	75.49	0.495	75.49	0.495
	90	90.49	0.492	88.99	1.007	90.49	0.492	90.49	0.492
LLL (ABC)	10	9.51	0.419	11.01	1.008	8.76	1.242	9.51	0.419
	25	26.01	1.001	26.01	1.001	24.51	0.495	24.51	0.495
	75	73.99	1.001	73.99	1.001	75.49	0.495	74.49	0.495
	90	89.74	0.258	88.88	1.007	90.49	0.492	90.49	0.492

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The percentage calculation of the error fault line to line to the ground fault shows that at 10 km and 90 km, long transmission lines Db4, Sym4 and Db8 had the same percentage of error. Conversely, at 25 km and 75 km, the percentage error of Sym4 and Db8 were less compared with Db4 and Coif4 since Coif4 had a major percentage of error in all cases. This indicates that the proposed algorithm for fault classification is accurate and precise.

Conclusion

When transformed into a wavelet, the determination of fault location using the Clarke transformation was very accurate, with an error of less than 2%. This was true even at a distance of 50 km, with an average error of 0.258% which was achieved for the time of bus A to the point of disturbance for the time achieved by bus B. From the above results, Db8 was found to be the best compared with other mother wavelets, with the fastest detection time at 0.00016 seconds and produced the smallest error in all types of interference. Meanwhile, the largest percentage error was produced by the mother wavelet Coif4.

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Authors:

Makmur Saini, Faculty of Electrical Engineering, Universiti Teknologi Malaysia, 81310 Johor Bharu, Johor, Malaysia. E-mail: makmur.saini@fkegraduate.utm.my.

Abdullah Asuhaimi Mohd Zin, Faculty of Electrical Engineering, Universiti Teknologi Malaysia, 81310 Johor Bharu, Johor, Malaysia E-mail: abdullah@fke.utm.my..

Mohd Wazir Mustafa, Faculty of Electrical Engineering, Universiti Teknologi Malaysia, 81310 Johor Bharu, Johor, Malaysia. E-mail: wazir.mustapa@fke.utm.my

Ahmad Rizal Sultan , Faculty of Electrical Engineering, Universiti Teknologi Malaysia, 81310 Johor Bharu, Johor, Malaysia. Rizal.sultan@fkegraduate.utm.my.